



# ***SVN-49 Signal Anomaly***

***Presented by Tom Stansell***

***GPSW POC: Lt. Col. James Lake, Ph.D.***

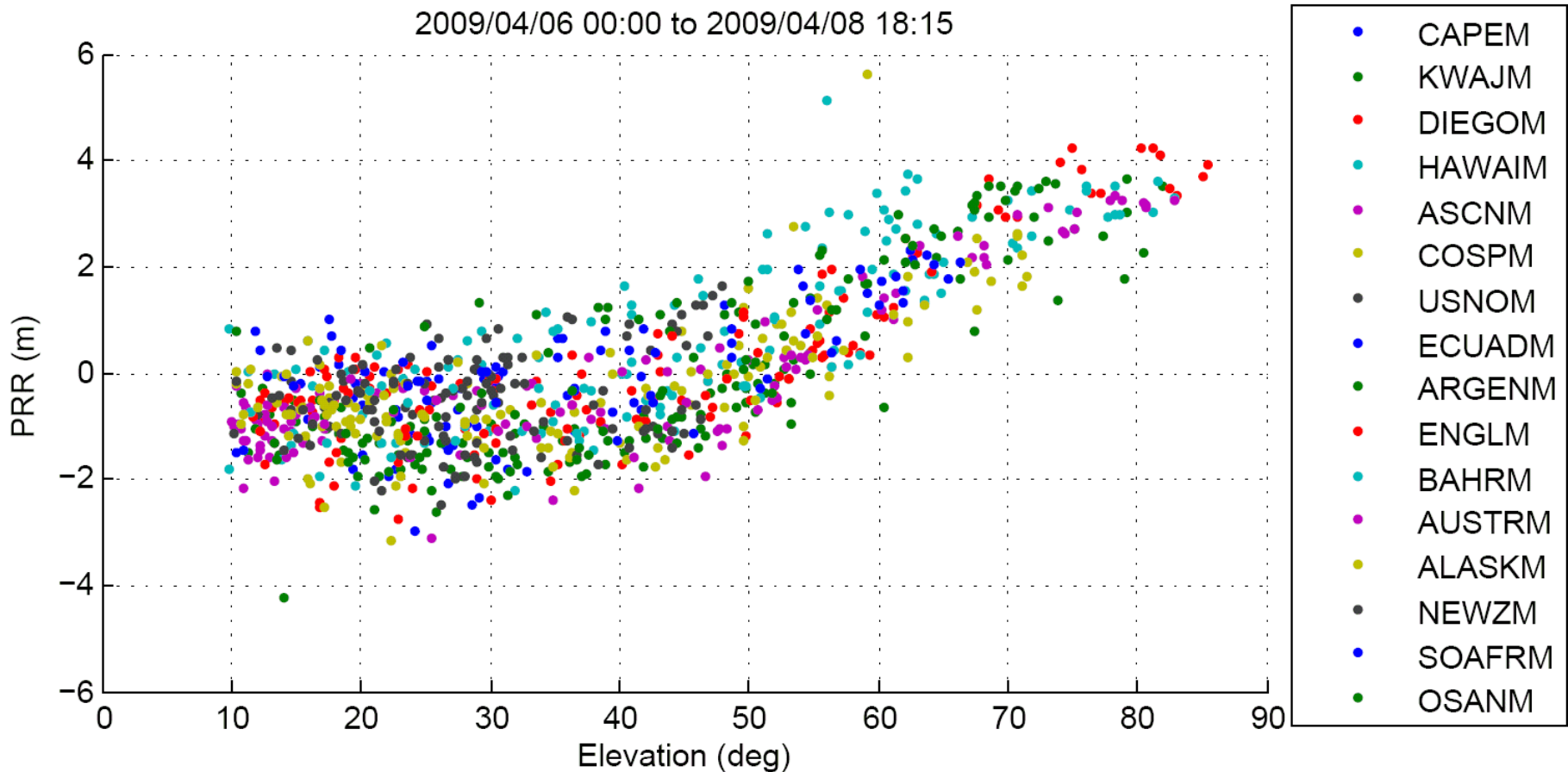


- **GPS IIR-20, SVN-49 (PRN 01), carries an L5 Demonstration Payload**
  - The L5 signal was not for operational use
  - The intent was to “bring L5 into use” for ITU purposes
- **The demonstration payload made use of an Auxiliary Payload port on the spacecraft**
- **No impact on the L1 and L2 signals was intended or expected**
- **However, 2SOPS and Aerospace reported unusually high and elevation angle dependent Pseudo Range Residuals (PRR) from the monitor stations**



# Pseudorange Residuals

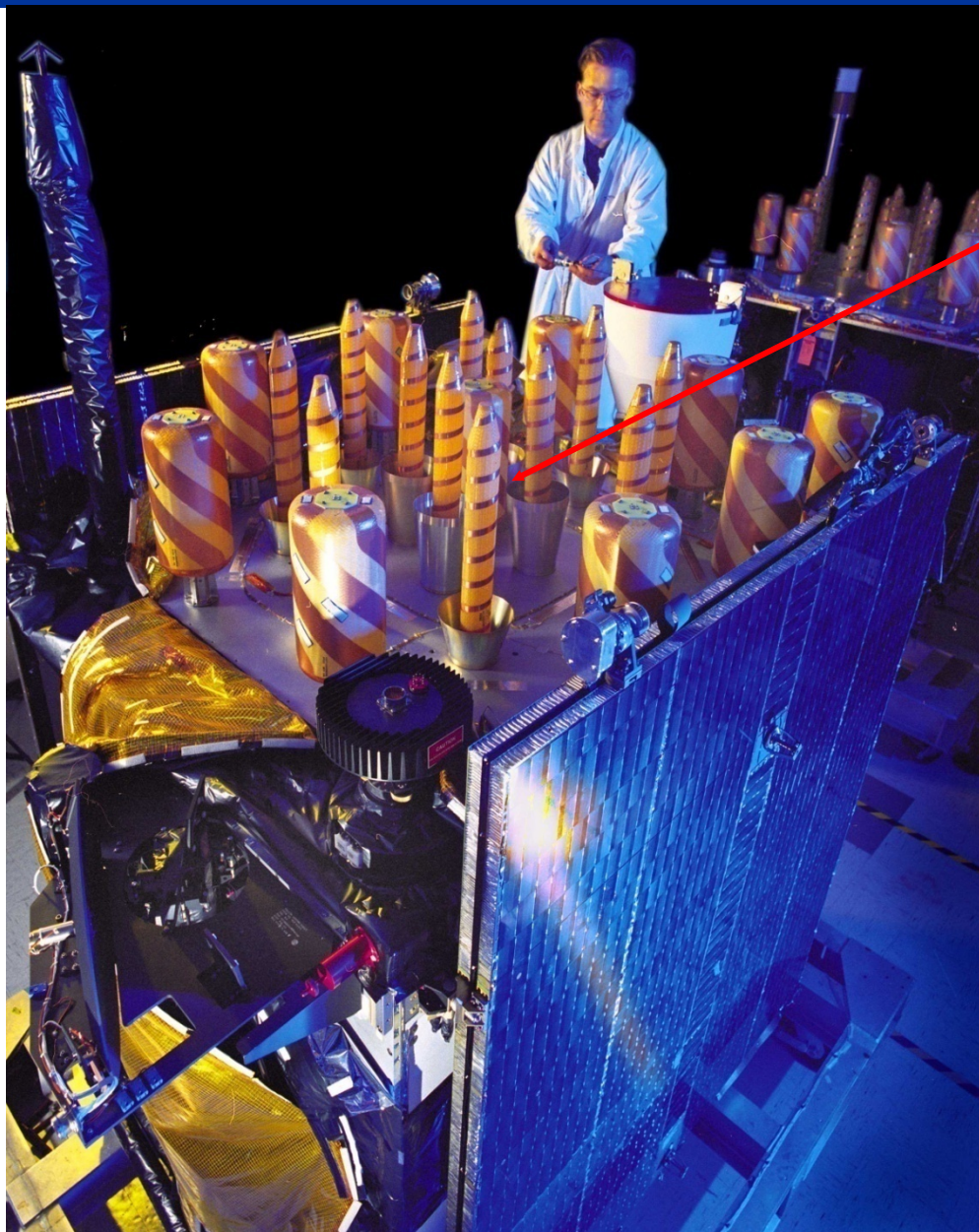
SVN49 PRR vs Elevation  
2009/04/06 00:00 to 2009/04/08 18:15



- Ionospheric refraction corrected pseudoranges
- Relative to a “best fit” orbit determined early in the test program
- Roughly a 4+ meter spread from 10 to 80 degrees



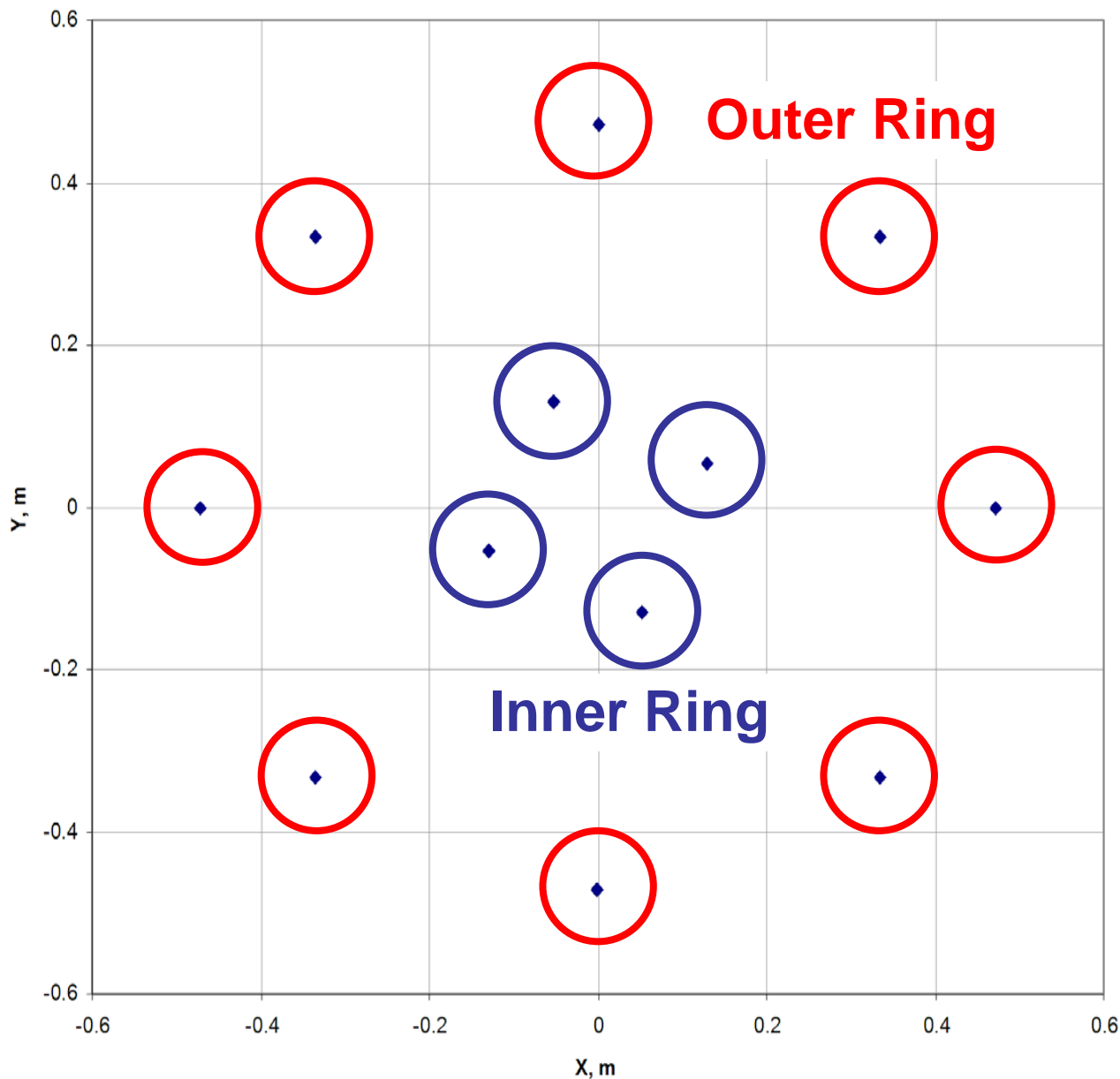
# GPS IIR Antenna Farm



L-Band Antenna  
Array with 12  
Helical Antennas

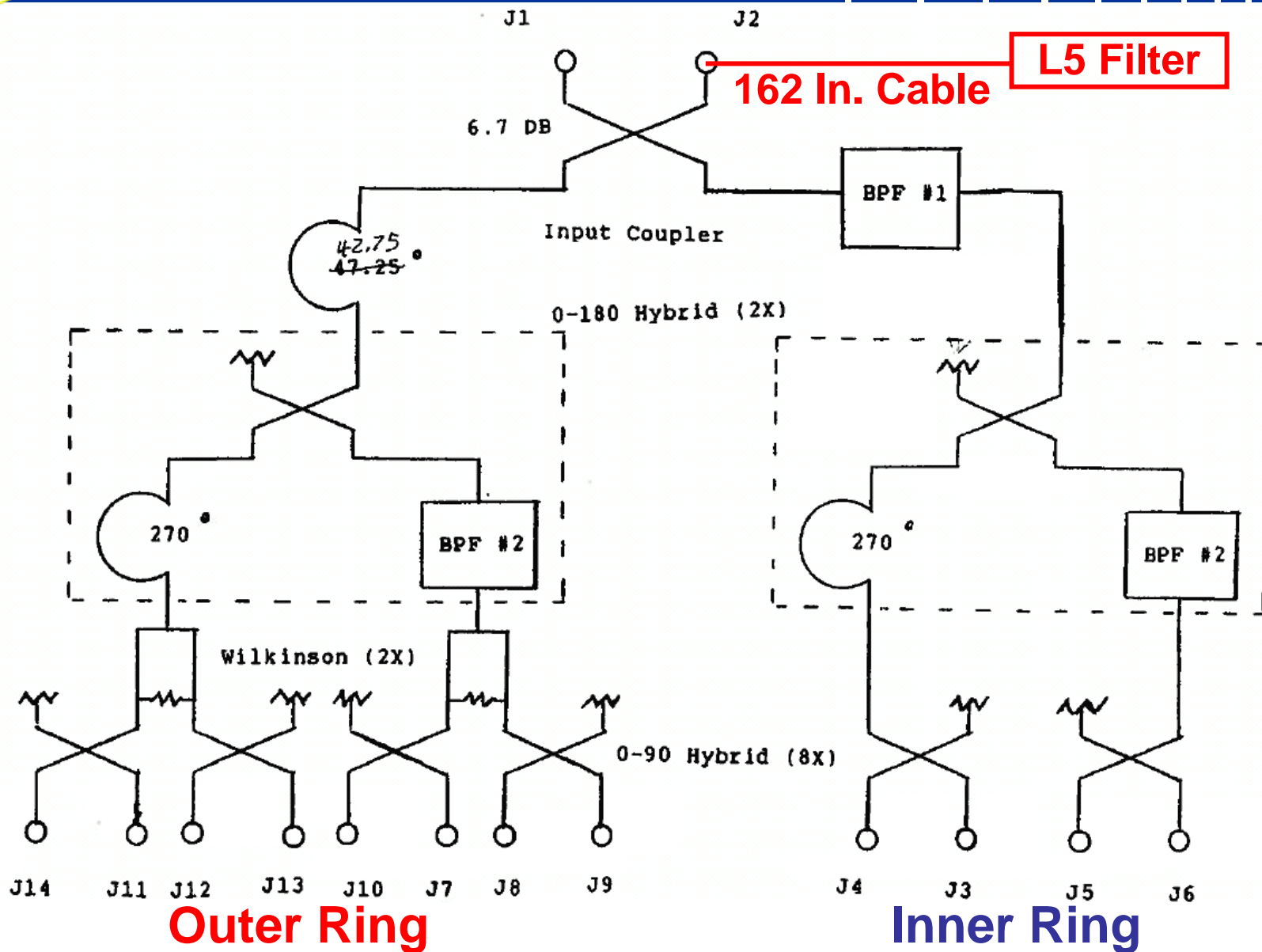


# L-Band Antenna Element Locations



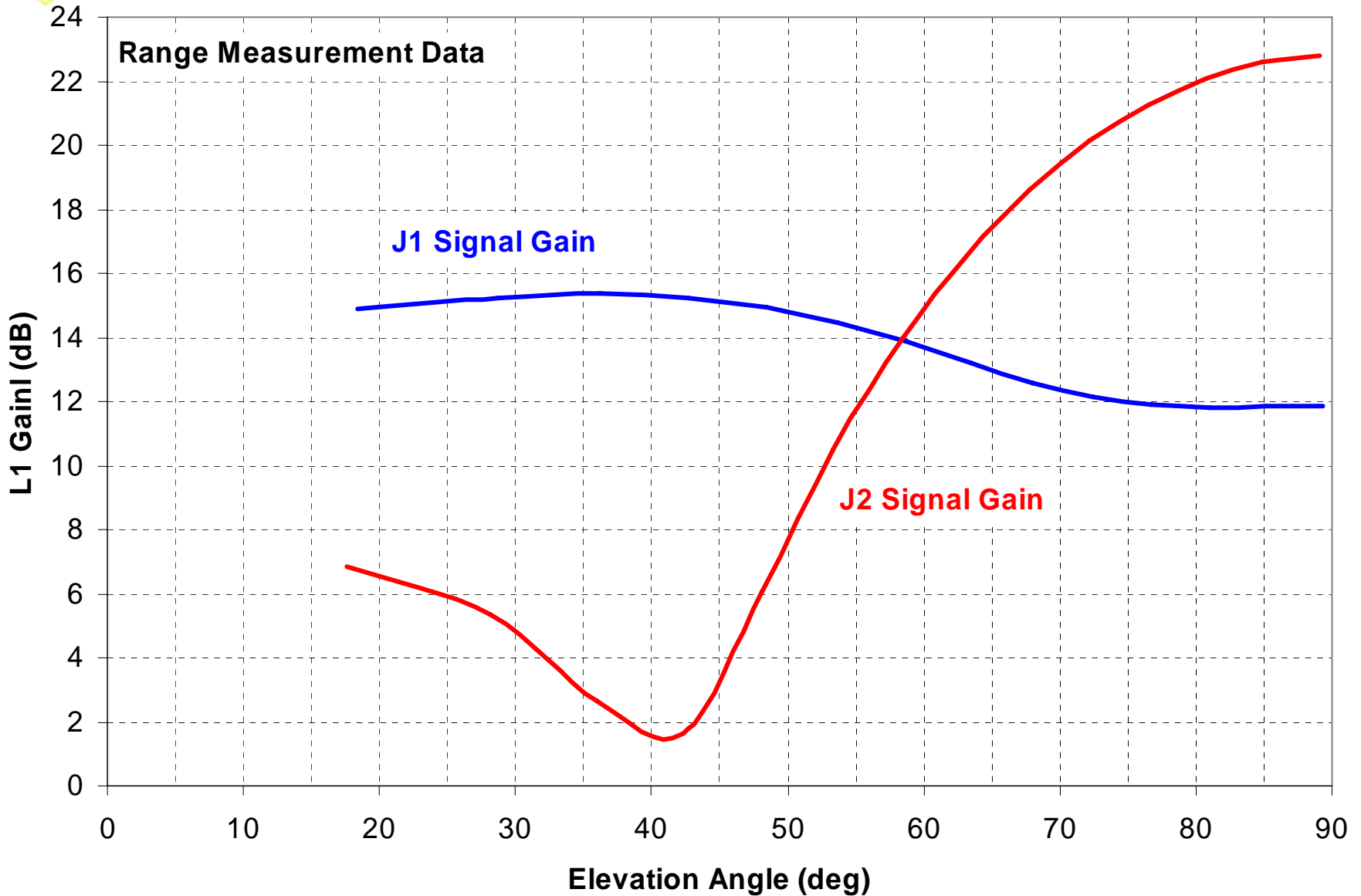


# Antenna Coupler Network



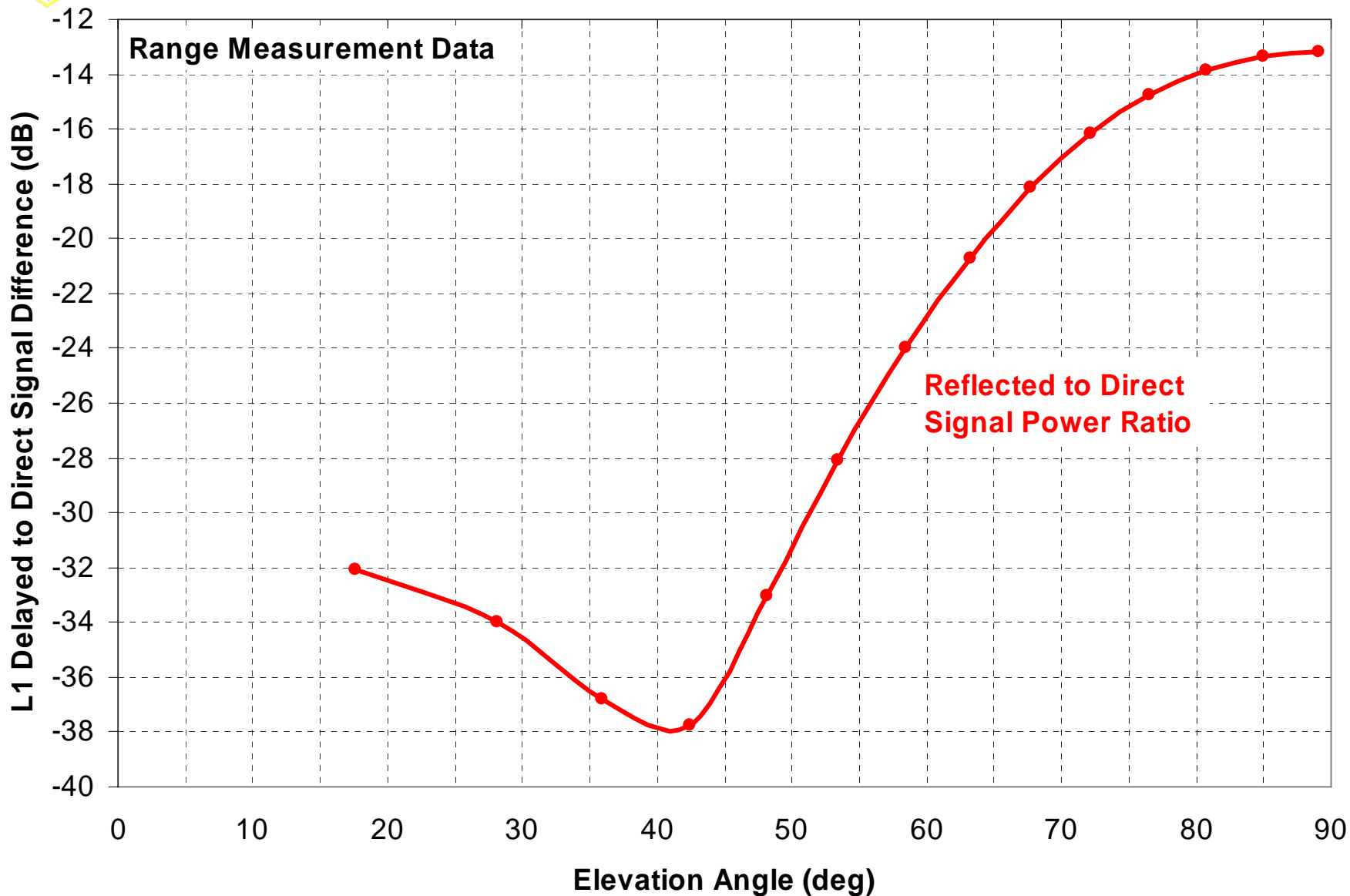


# J1 and J2 Antenna Patterns at L1





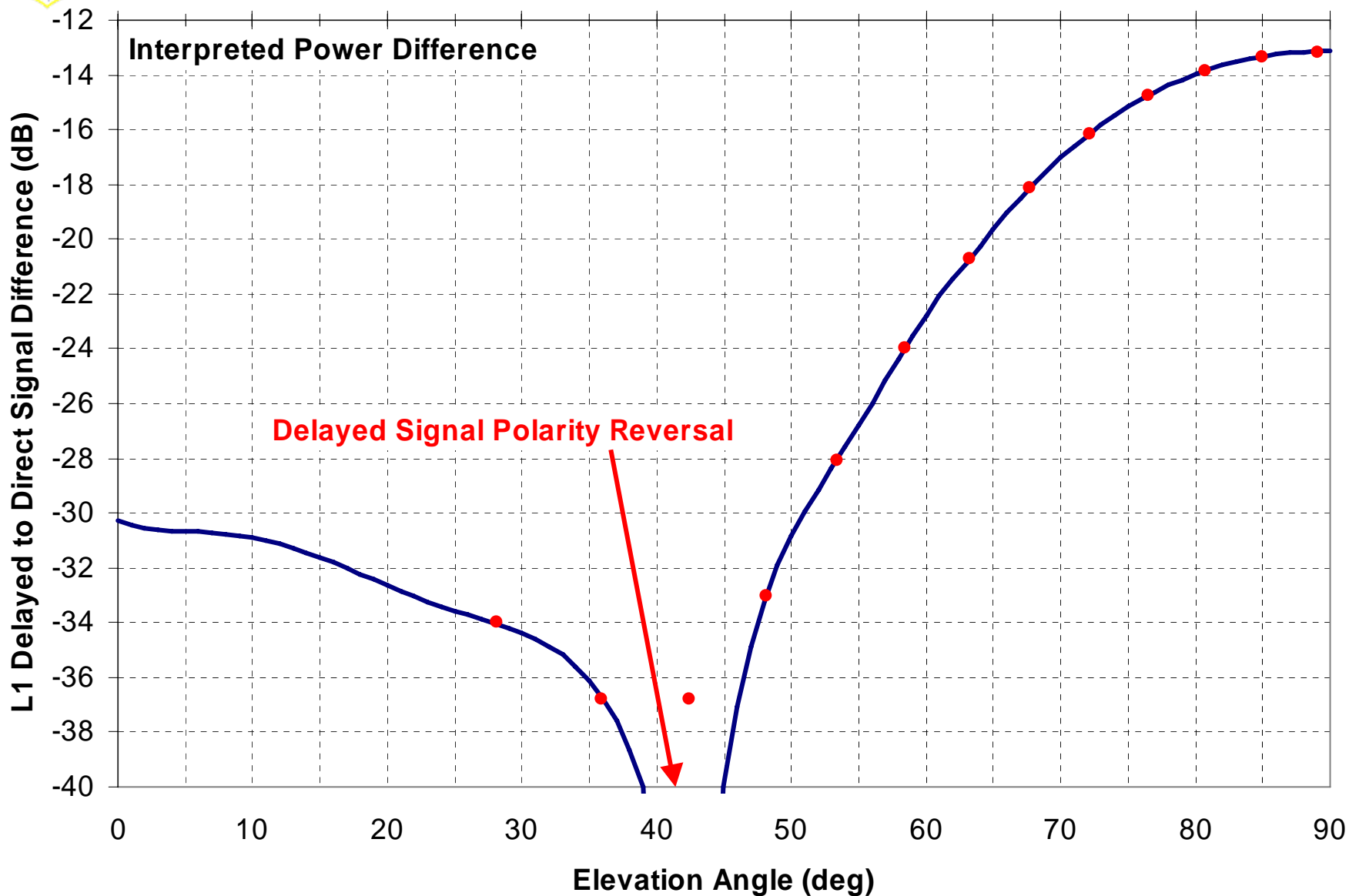
# Reflected Relative to Direct L1 Signal Power







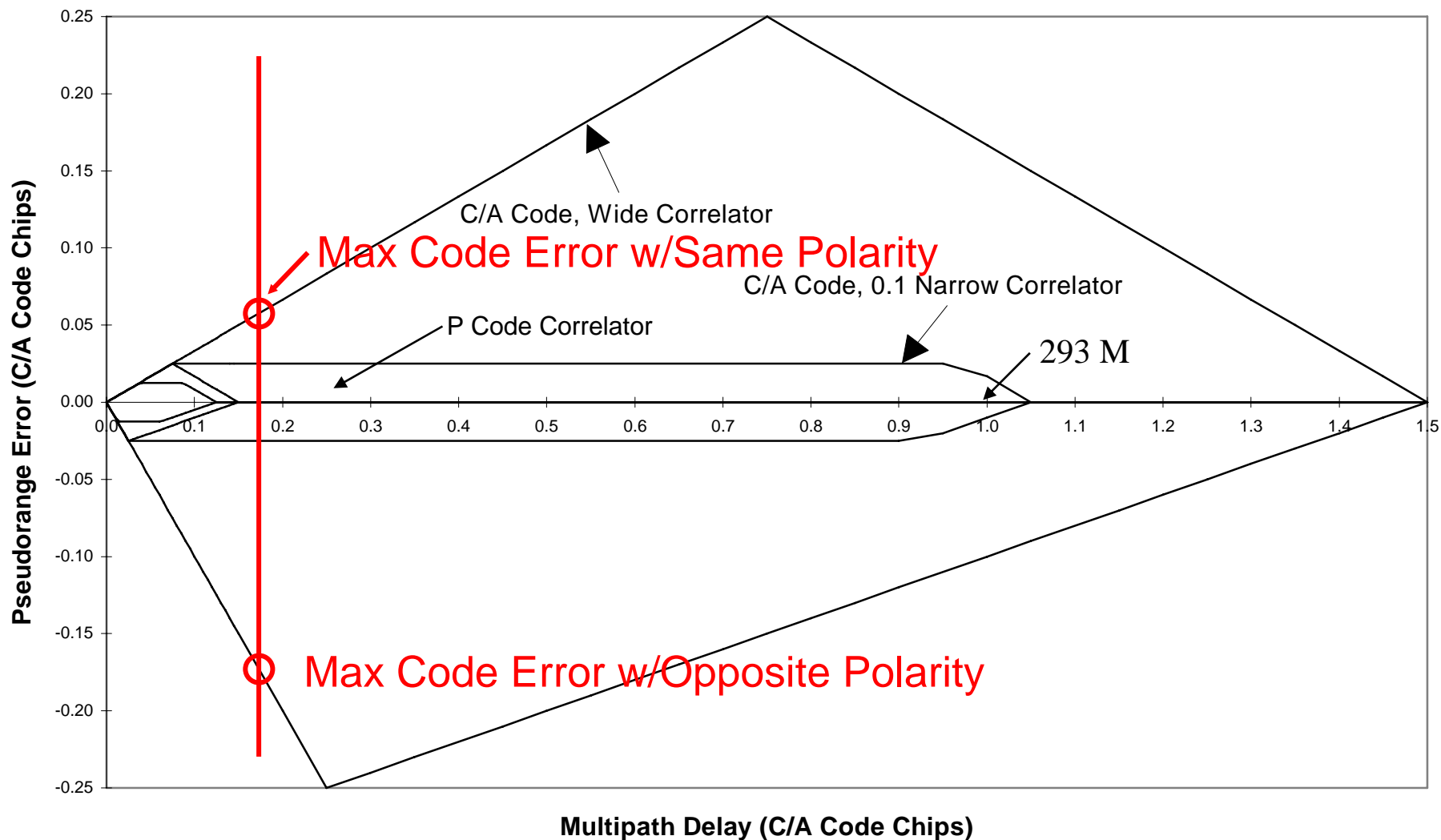
# Model of L1 Signal Difference





# Early Minus Late Tracking

## Effect of Half Voltage Amplitude Multipath Signal - C/A Code Scale





# Ionospheric Refraction Calculation

$$L1 / L2 = 1575.42 / 1227.6 = 77 / 60$$

$$77^2 = 5929$$

$$60^2 = 3600$$

$$77^2 - 60^2 = 2329$$

$$PR = (PR_{L1} \cdot 77^2 - PR_{L2} \cdot 60^2) / (77^2 - 60^2)$$

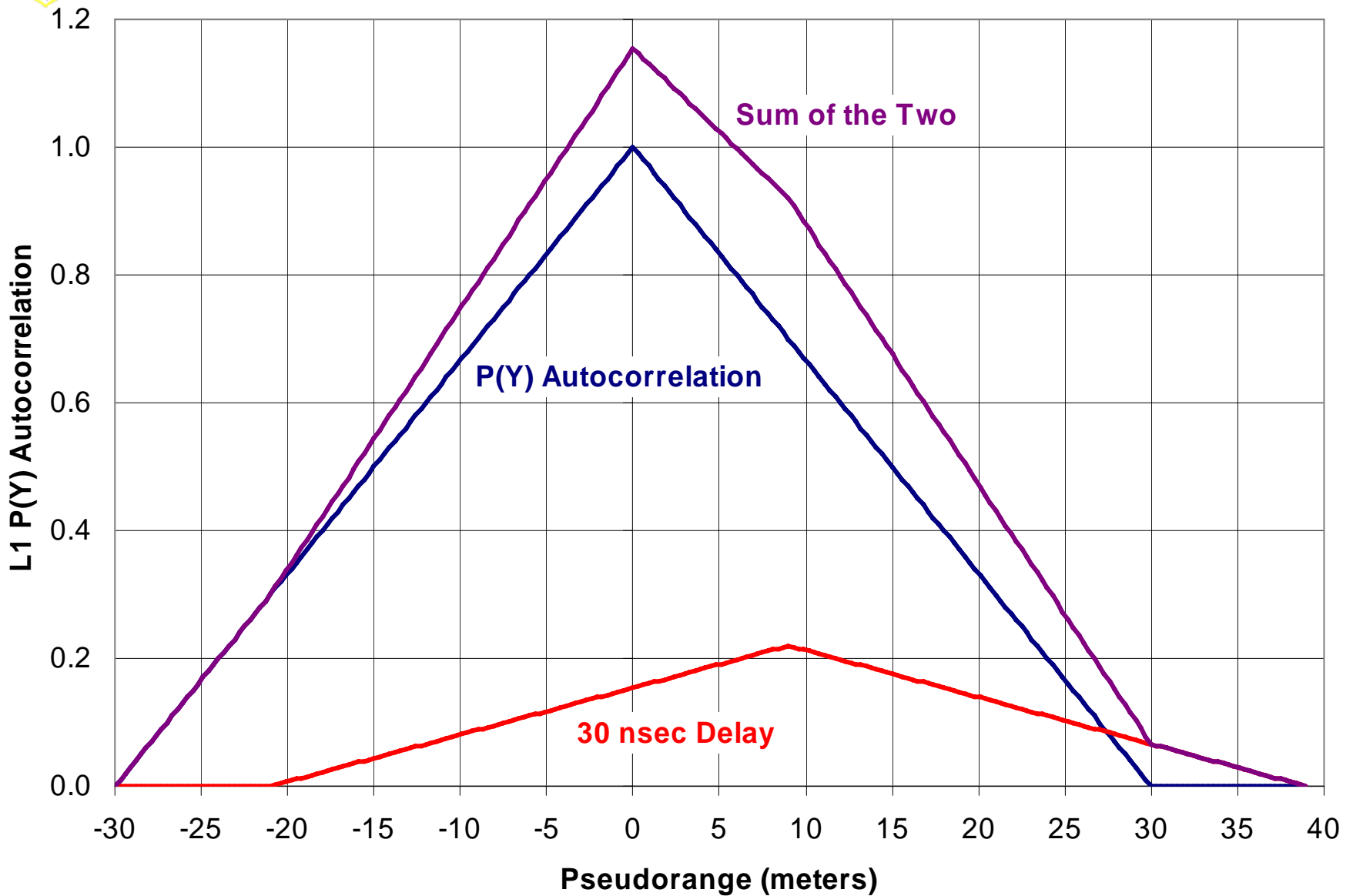
$$PR \approx 2.55 PR_{L1} - 1.55 PR_{L2}$$

$$\sqrt{2.55^2 + 1.55^2} = 2.984\dots \approx 3$$

Ionospheric correction amplifies code noise

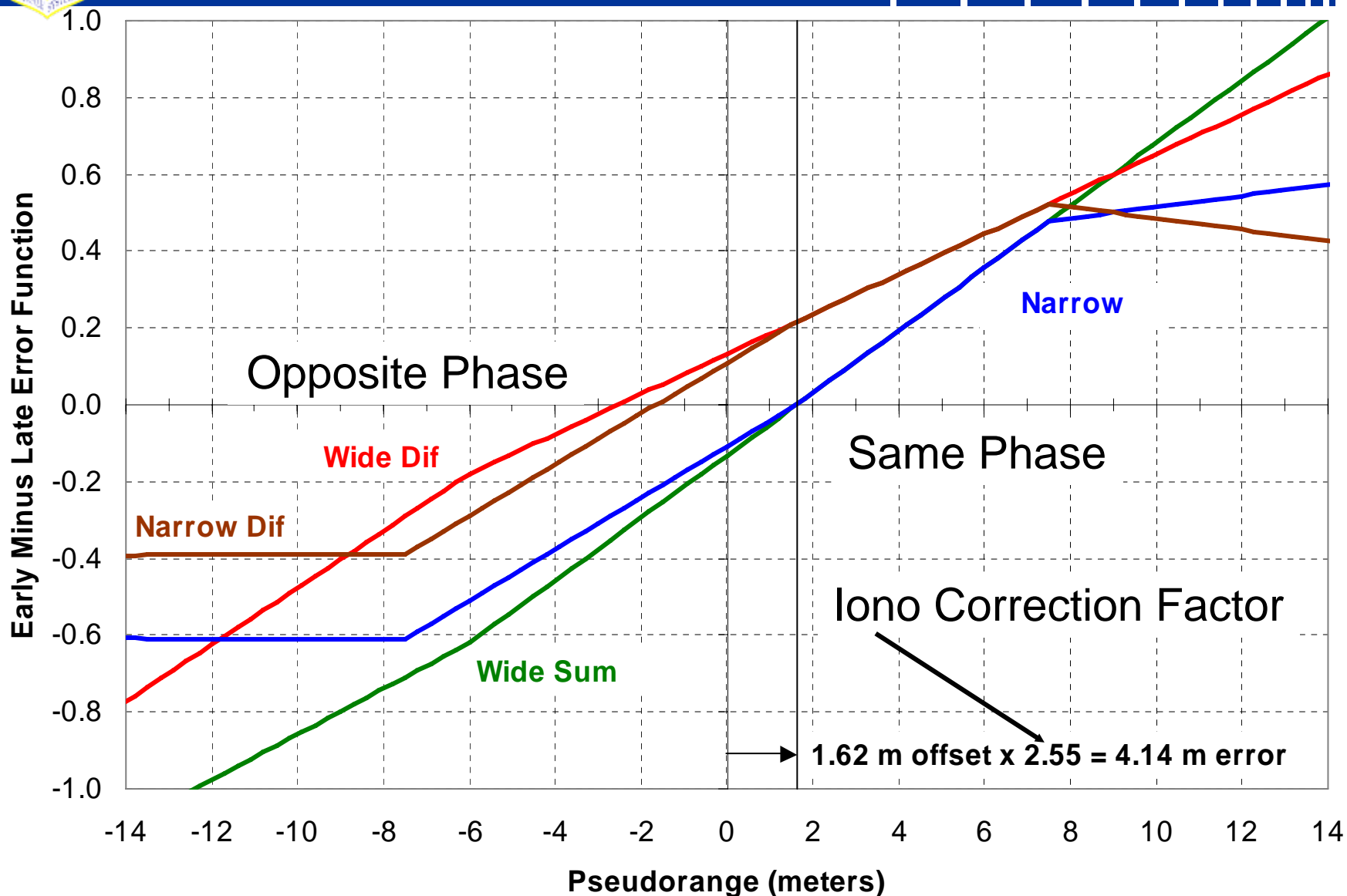


# Max Impact on L1 P(Y) Autocorrelation





# Early Minus Late L1 P(Y) Code Track Error



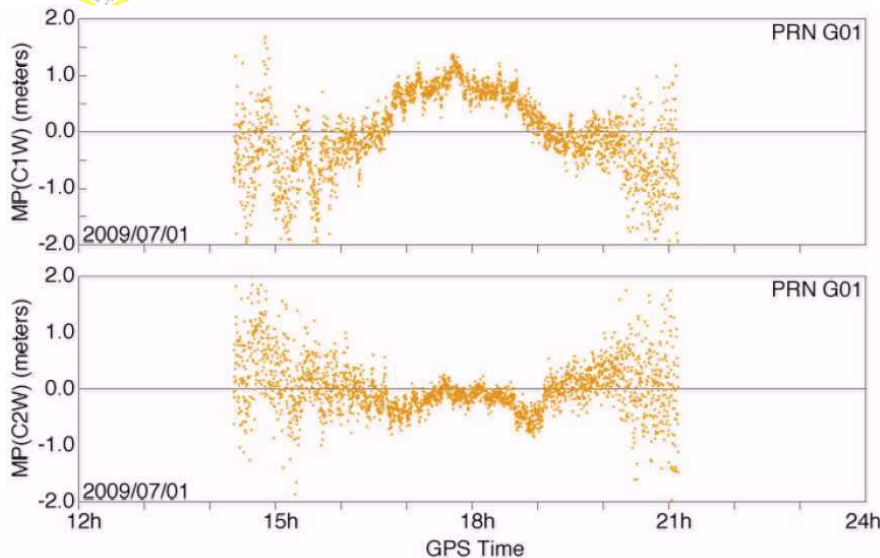


## *Useful Observation*

- **Receivers with early minus late correlators having similar spacing will have essentially the same tracking error for all signals at one frequency**
  - e.g., L1 P(Y) and L1 C/A exhibit the same error
- **However, different types of correlators and different correlator spacings very likely will produce different tracking errors**
  - See next slide with figures from 13 July '09 GPS World Article



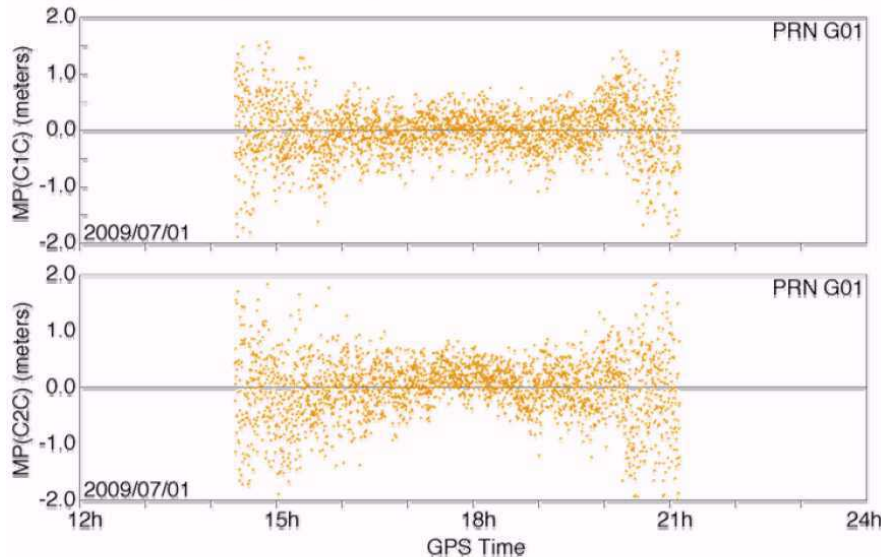
# Tracking Error with Different Correlators



L1 Typical Semi-Codeless Correlator

L2 Typical Semi-Codeless Correlator

FIGURE 4. Typical SVN49 multipath errors for semi-codeless P(Y)-code tracking on L1 (top) and L2 (bottom) from a conventional correlator.



L1 Using Multipath Mitigation w/  
20 nanosecond correlator spacing

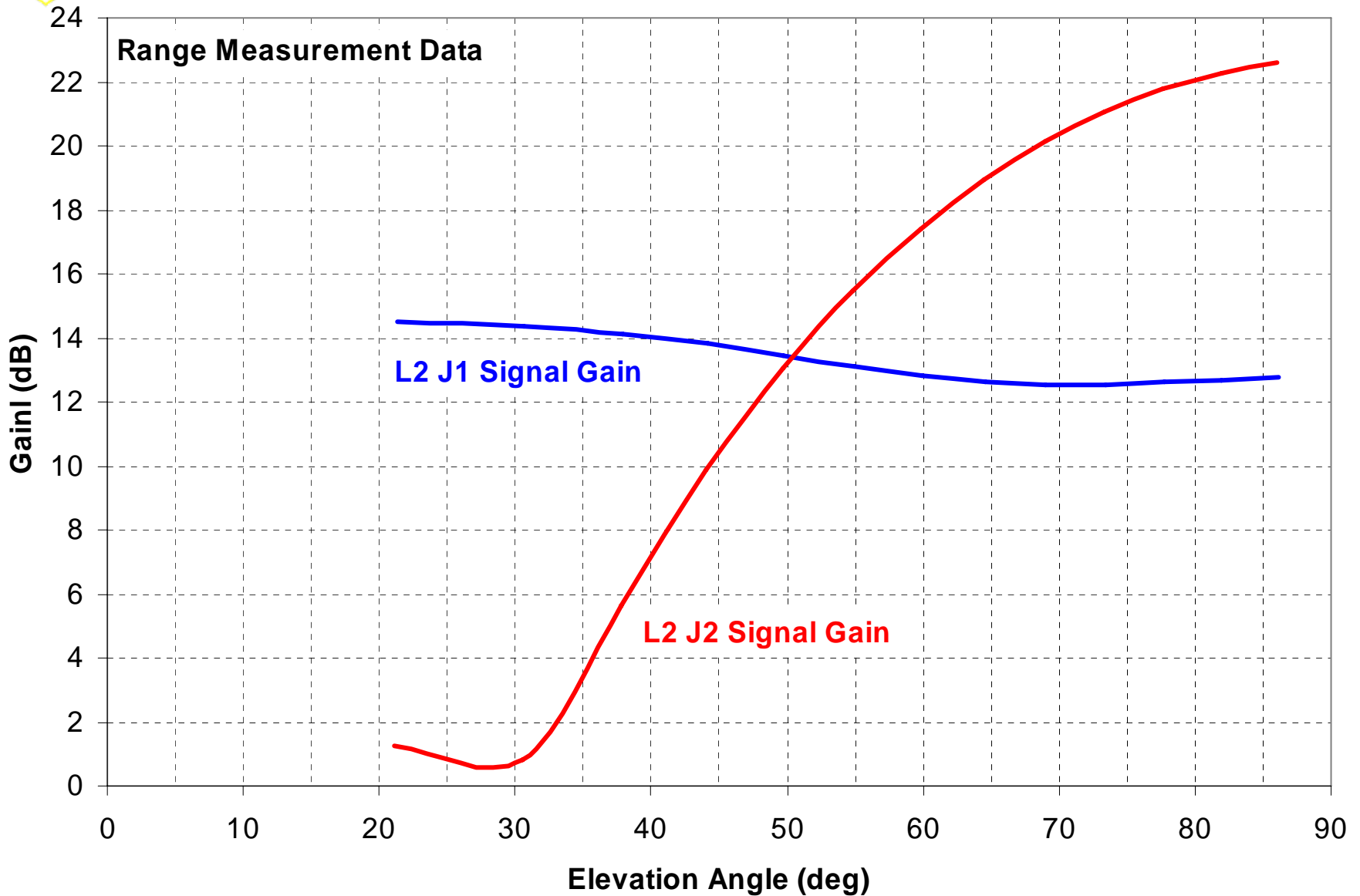
L2 Using Multipath Mitigation w/  
20 nanosecond correlator spacing

FIGURE 5. SVN49 multipath errors for C/A-code (top) and L2C-code (bottom) tracking using special multipath-mitigation techniques with 20-nanosecond correlator spacing

Figures courtesy of GPS World, receivers are JAVAD GNSS Triumph receivers



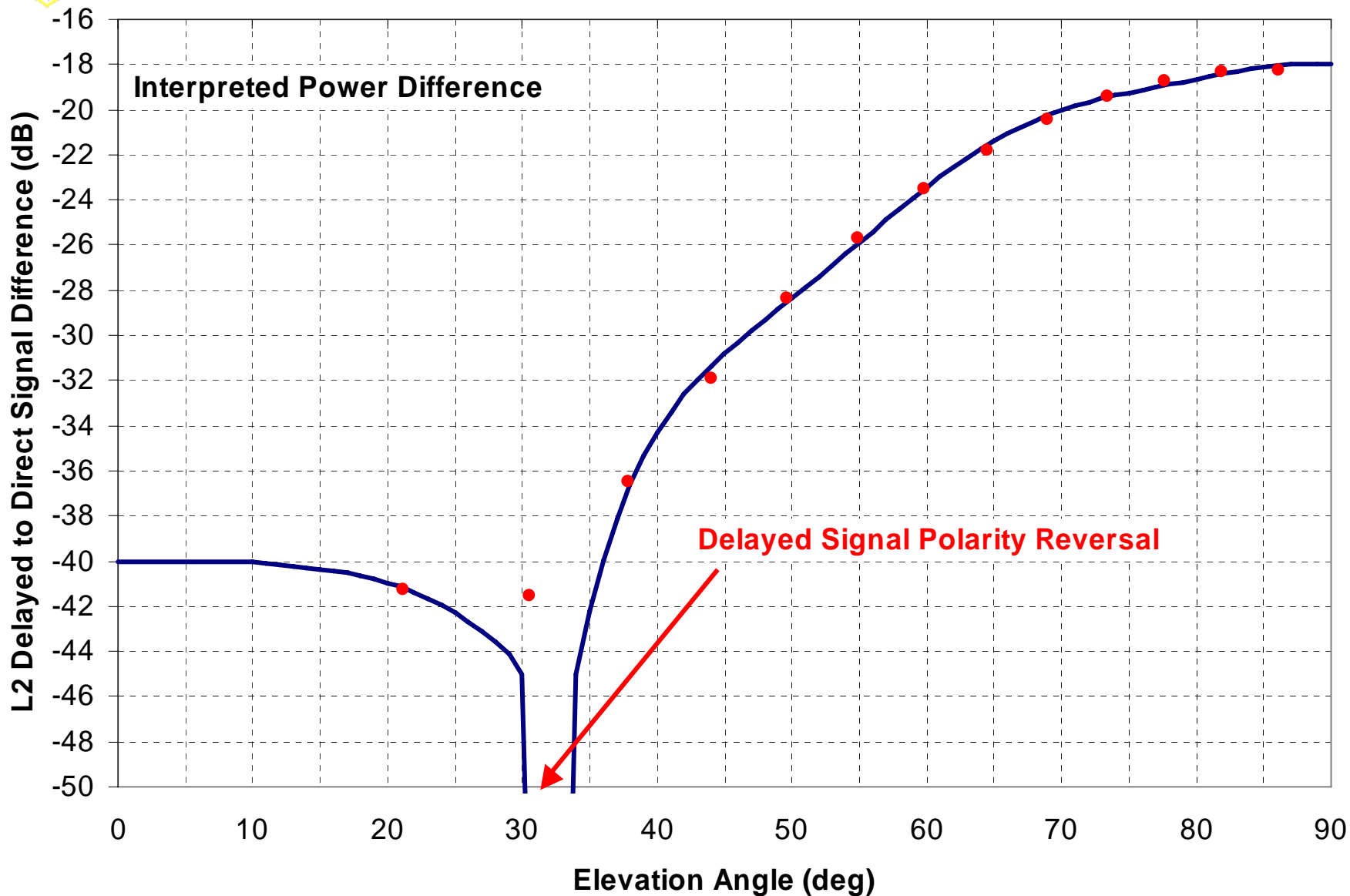
# J1 and J2 Antenna Patterns at L2





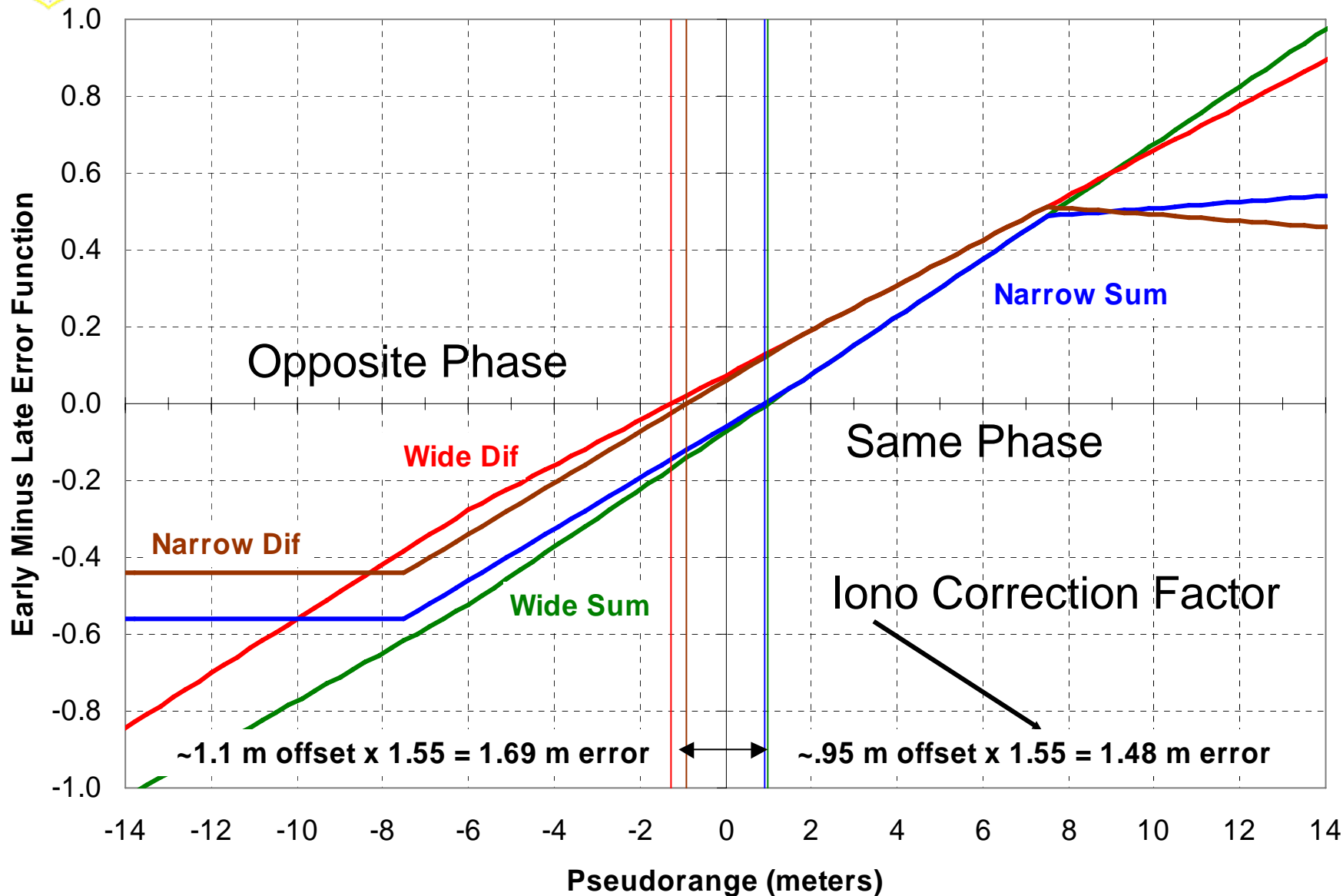


# Model of L2 Signal Difference





# Early Minus Late L2 P(Y) Code Track Error



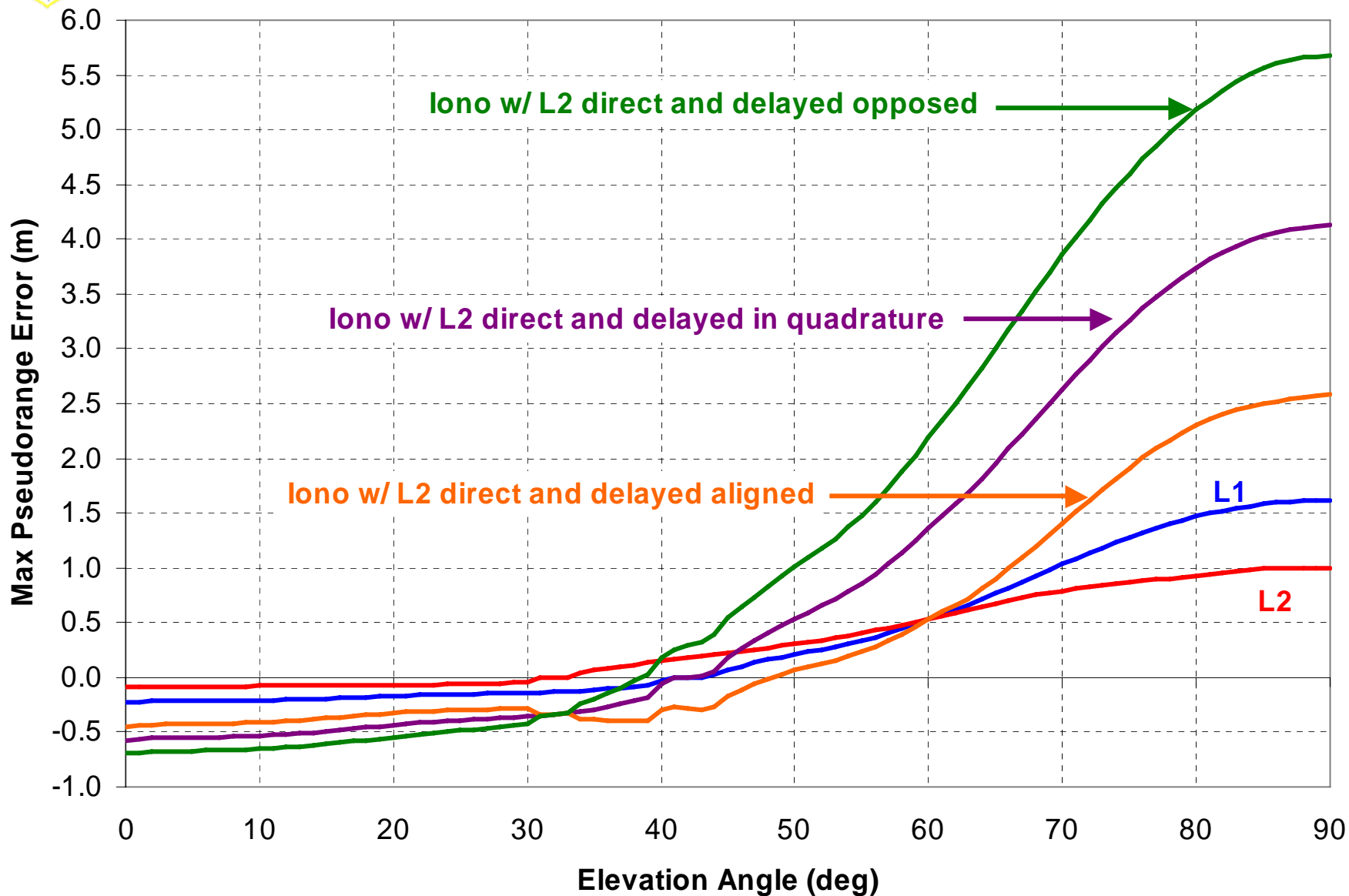


## ***Refraction Corrected Error Possibilities***

- Assume the direct and reflected L1 signals are in phase so at zenith the L1 pseudorange is 1.62 m too long
- If the direct and reflected L2 signals are in quadrature, the L2 pseudorange error is negligible
- Therefore, the refraction corrected pseudorange error is  **$(2.55 \times 1.62 - 1.55 \times 0) = 4.14 \text{ m}$**
- If the direct and reflected L2 signals are in the same phase, the L2 pseudorange error is  $\sim 0.95 \text{ m}$
- Therefore, the refraction corrected pseudorange error is  **$(2.55 \times 1.62 - 1.55 \times 0.95) = 2.66 \text{ m}$**
- If the direct and reflected L2 signals are in opposite phase, the L2 pseudorange error is  $\sim -1.1 \text{ m}$
- Therefore, the refraction corrected pseudorange error is  **$(2.55 \times 1.62 - 1.55 \times -1.1) = 5.84 \text{ m}$**

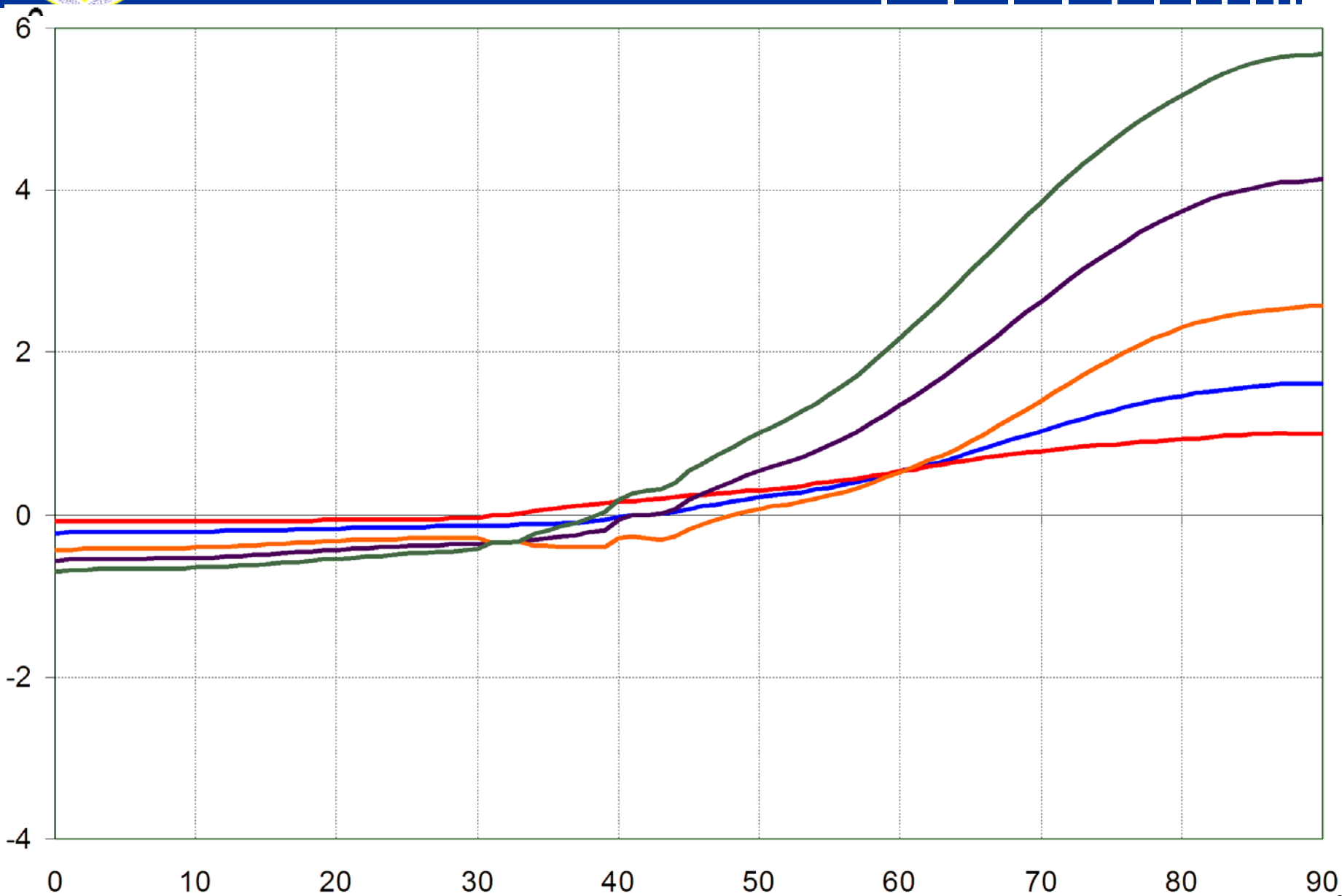


# Pseudorange Error Model





# Curves and Residuals Overlay



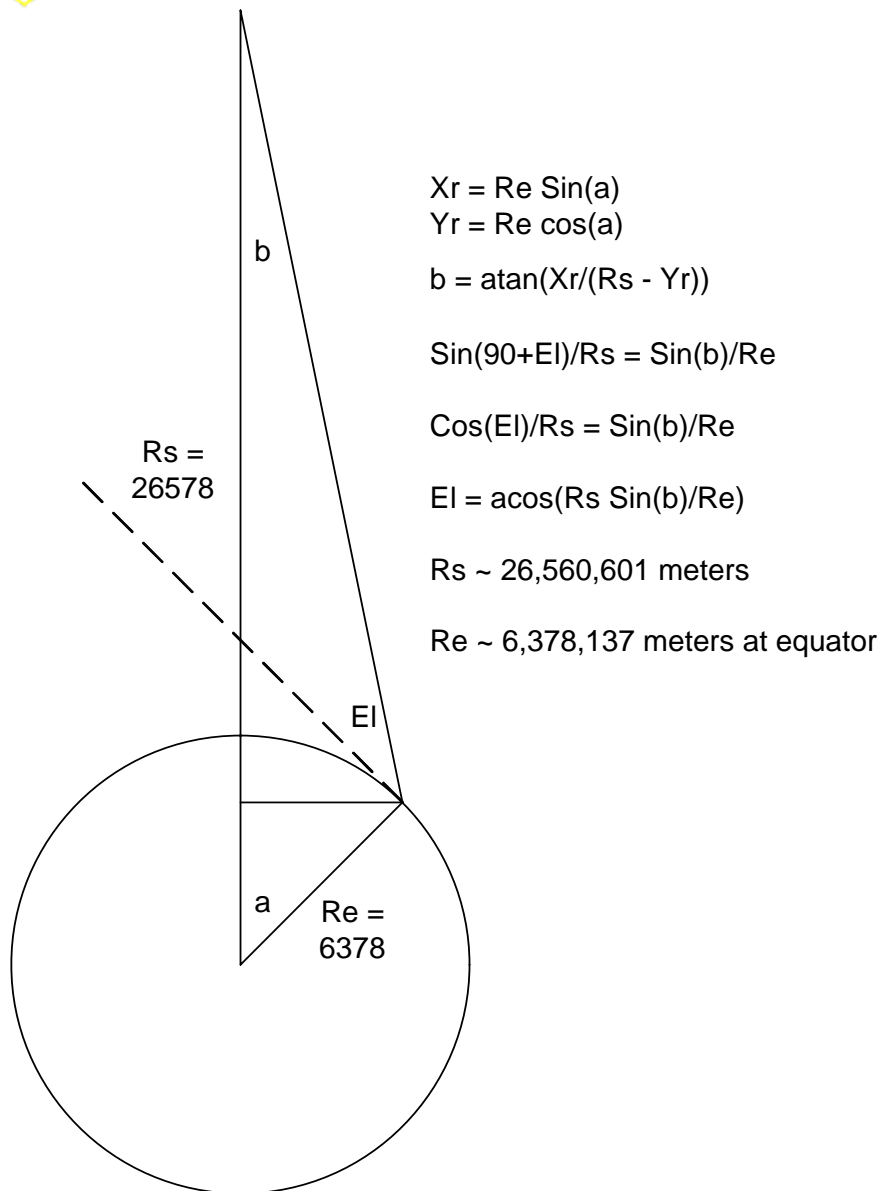


## *A Partial Fix*

- **In order to reduce the elevation-dependent tracking residuals, 2SOPS has experimented with placing the antenna phase center about 152 meters above the satellite rather than slightly below as normal**
  - (How can you fix a 4-5 meter problem with a 152 meter solution?)
- **The Kalman filter then provides orbit and clock parameters which best fit the tracking data**
  - The key parameter is clock offset
- **Over the next few weeks, different values will be tried and transmitted in the NAV messages**



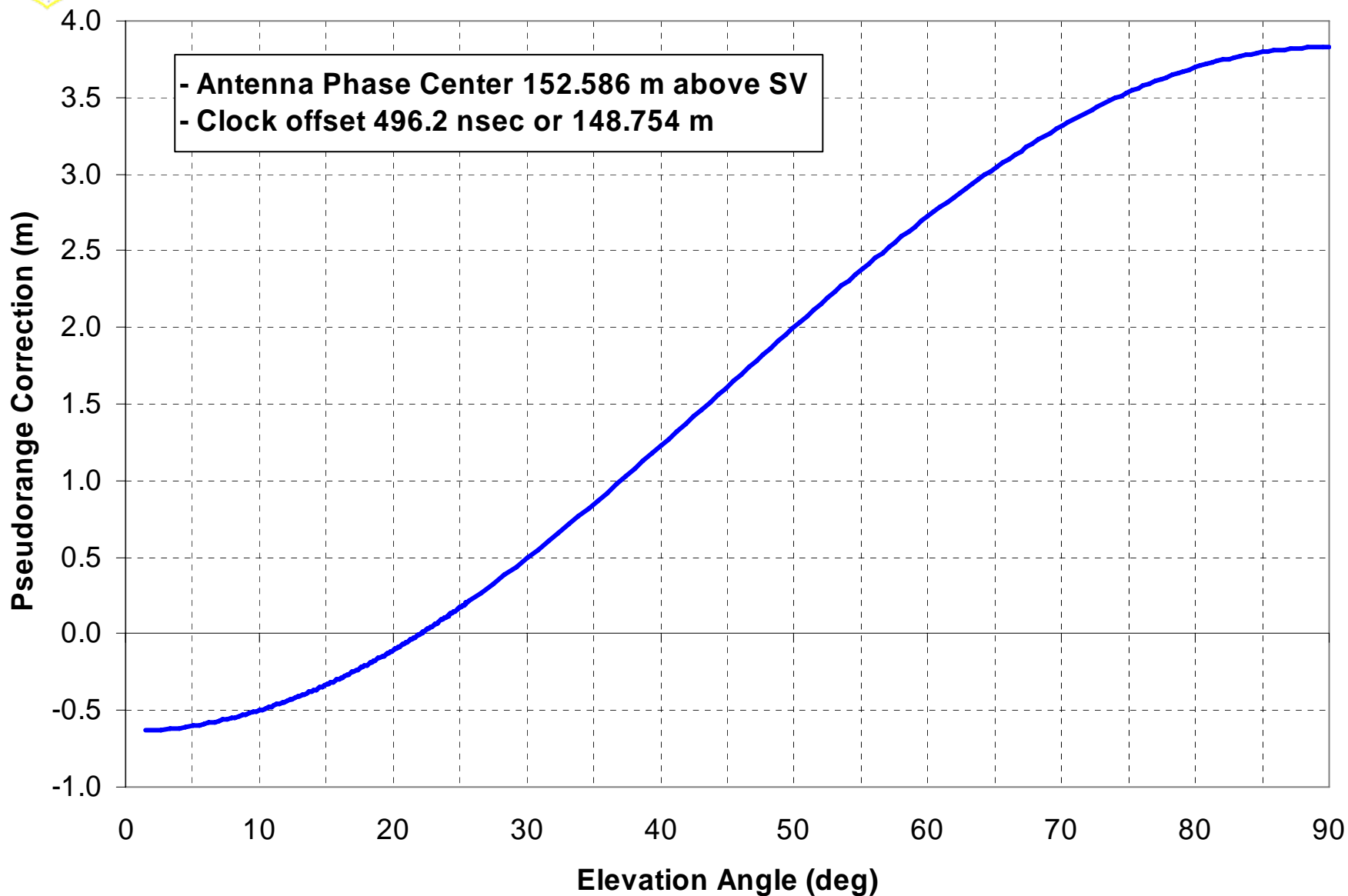
# Raise the Orbit, Offset the Clock



- If  $R_s \text{ effective} = R_s + \delta$
- The impact on pseudorange is  $\delta \cos(b)$
- The following plot shows the effect of  $\delta = 152.586$  m with a clock offset of 496.2 nsec (148.754 m)



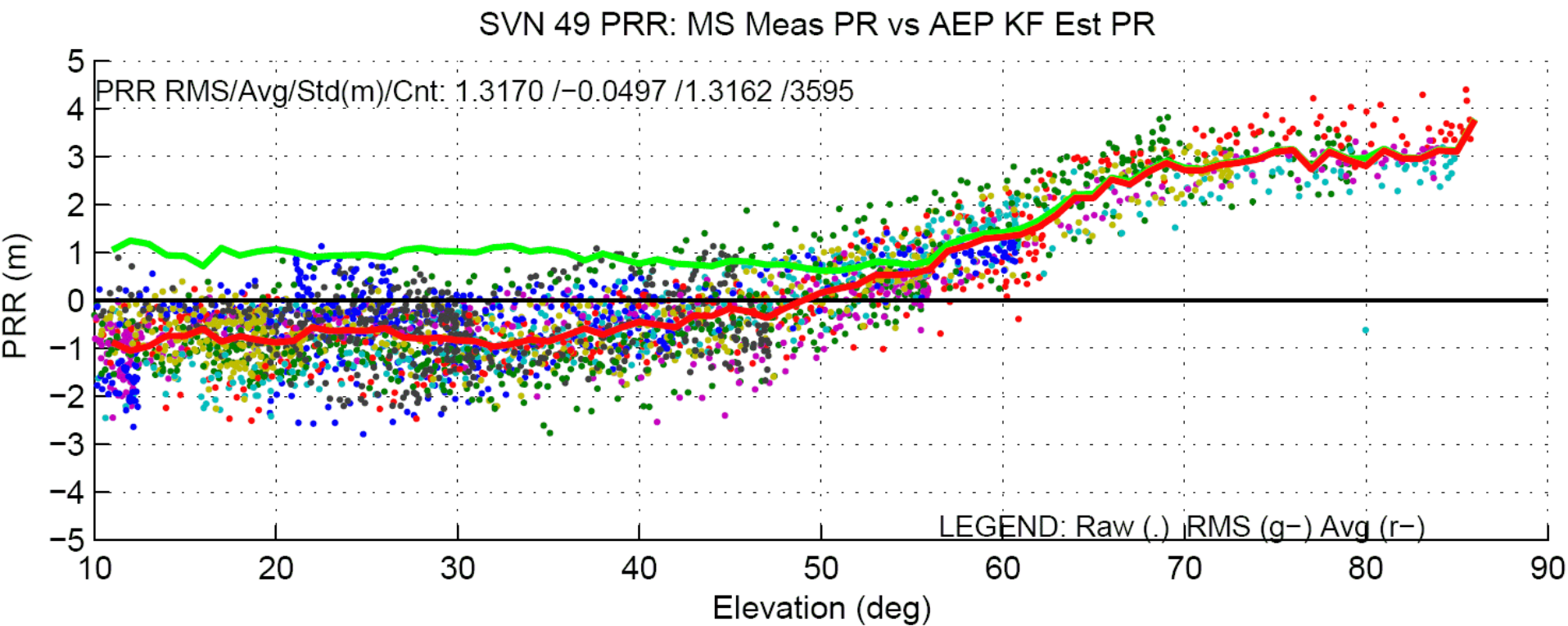
# Net Compensation





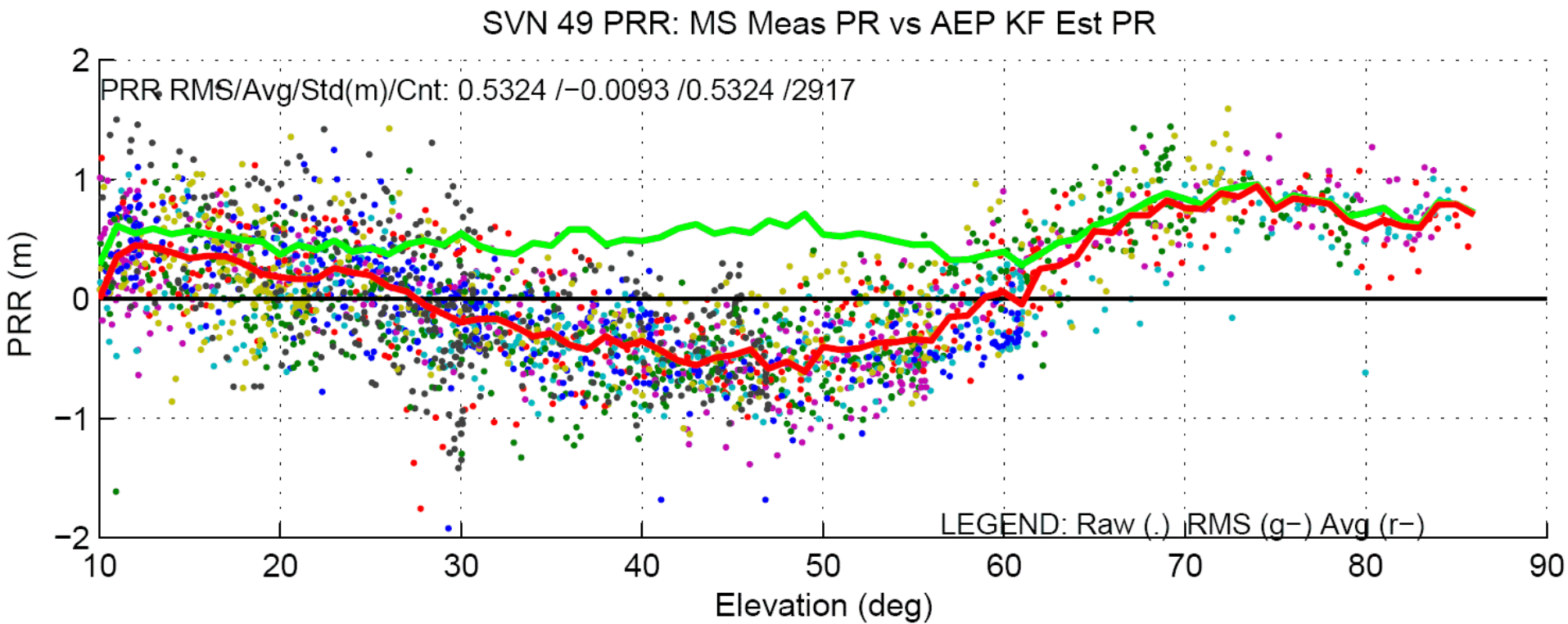


# Uncompensated Residuals



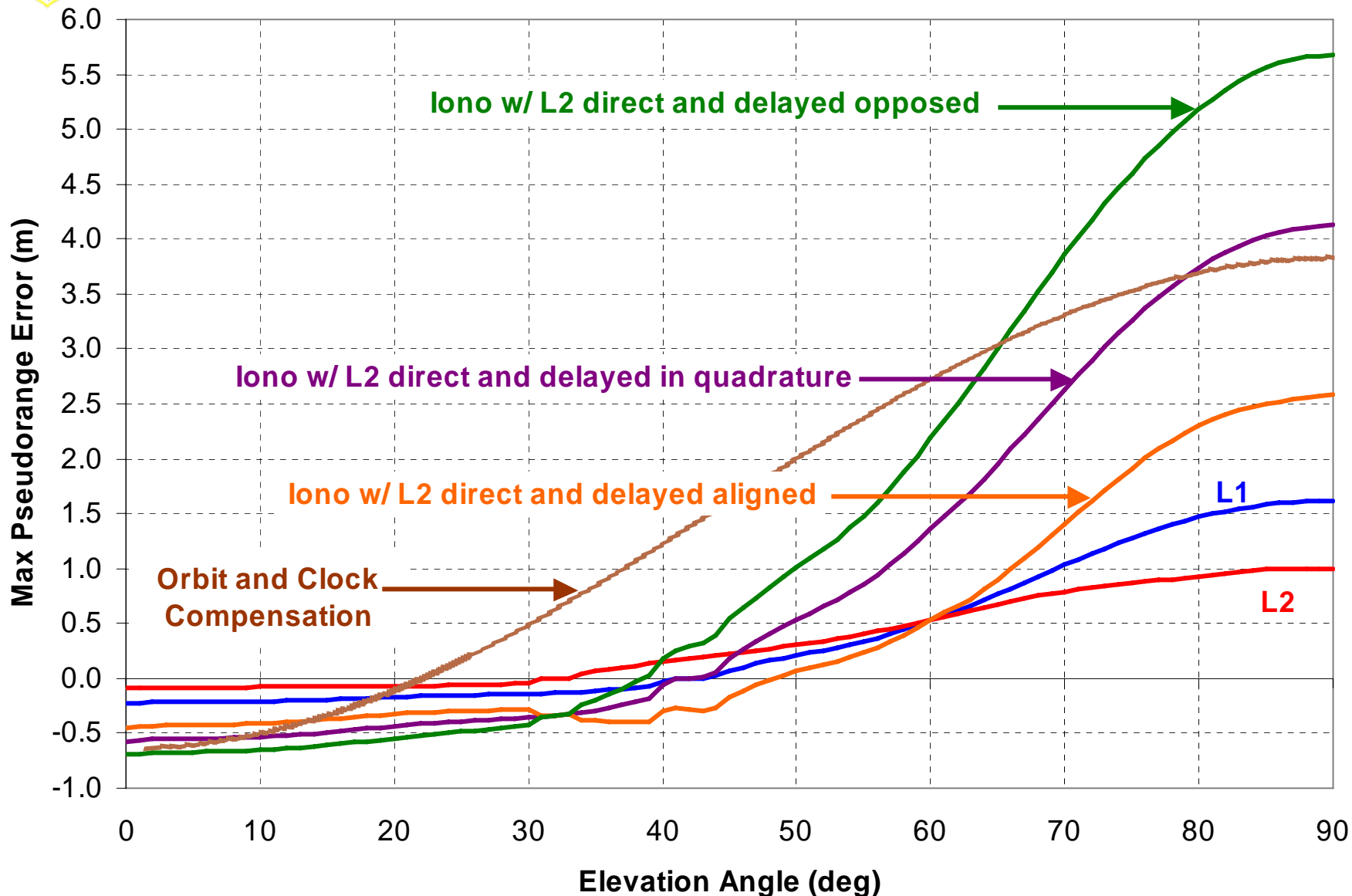


# Compensated Residuals





# Compare Compensation with Error Models





# *Spirent Simulation*

- **Note for organizations with a Spirent simulator**
  - Spirent is preparing a scenario, based on these models, to simulate the SVN-49 problem and enable laboratory testing
  - The scenario provides normal L1 and L2 signals plus a delayed signal with the proper relative amplitude and phase relationships as a function of elevation angle in accordance with these models
  - Several parameters can be modified by the operator
  - The scenario will available directly from Spirent by request